

Development of space compatible Polarization Modulator

Yuki Sakurai (Kavli IPMU, The University of Tokyo)
and LiteBIRD PMU development team



B-mode from space 2019 at Munich
Dec. 19, 2019



東京大学
THE UNIVERSITY OF TOKYO



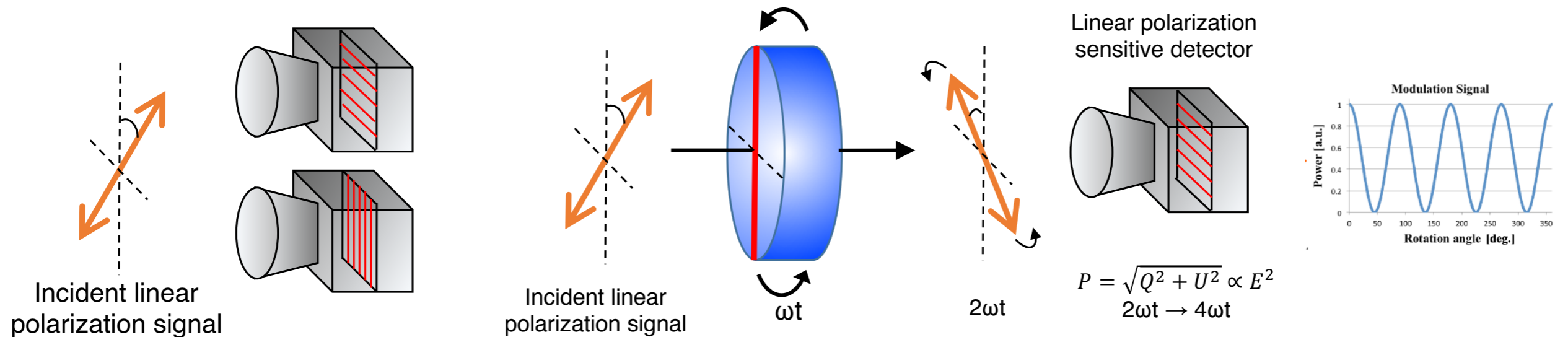
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研究拠点形成事業
Core-to-Core Program



What is polarization modulator?

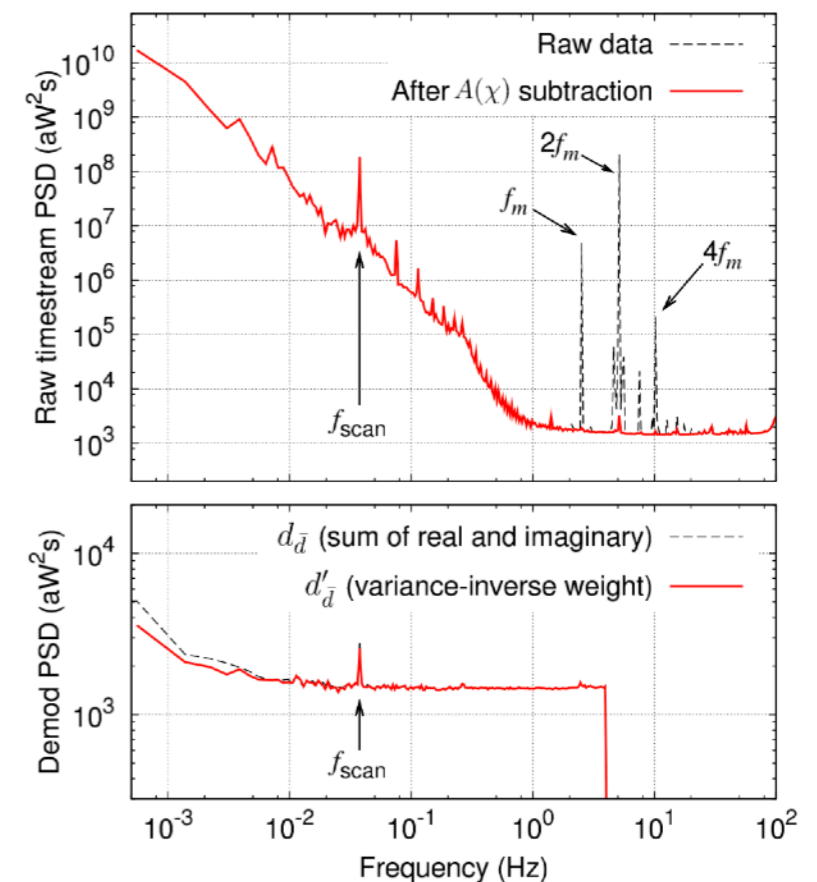


1. 1/f noise rejection

- ✓ Atmospheric noise, ground pickup
- ✓ Detector / electrical noise
- ✓ Long term instabilities

2. Systematics mitigation

- ✓ Differential beam pointing, ellipticity
- ✓ Differential gain

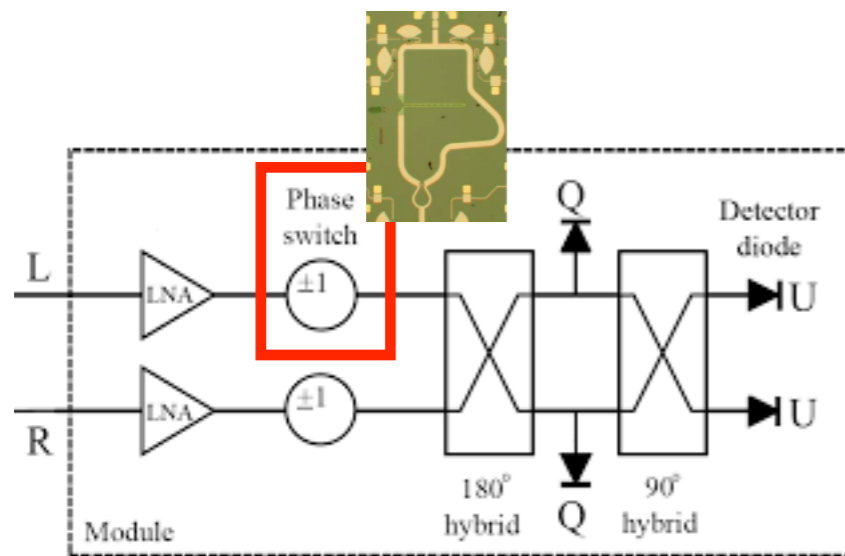


A. Kusaka et al., 2014

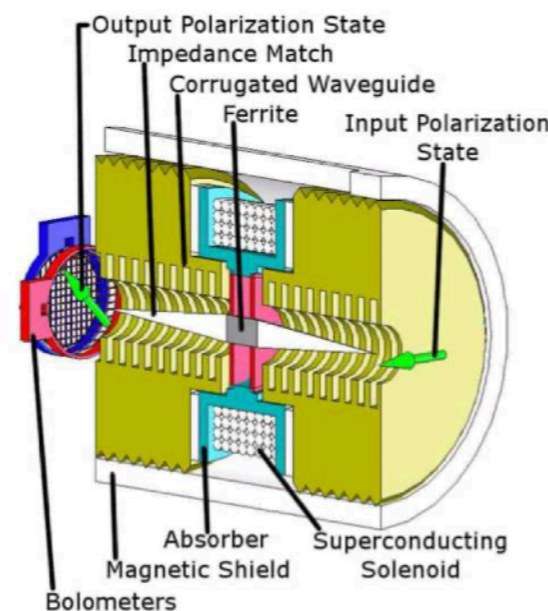
Modulation techniques

There are various polarization modulation techniques:

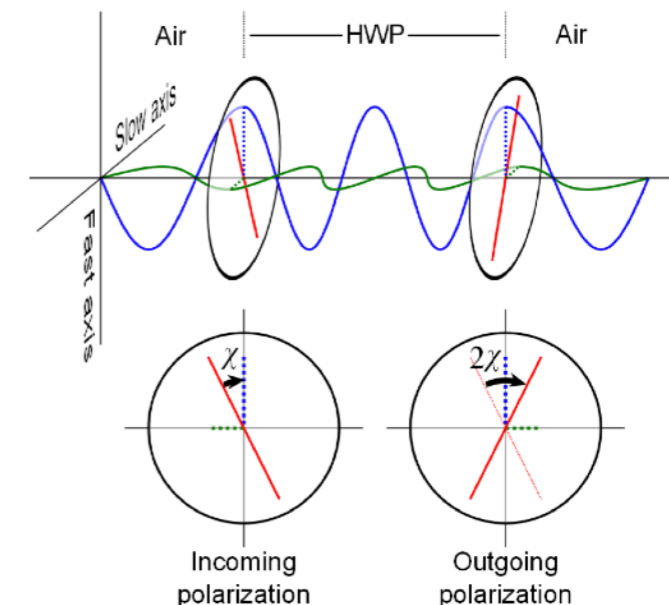
1. **Phase switch:** WMAP, CAPMAP, QUIET...
 - Modulation by switching the path length half-phase shifted ➔ Install at front or rear of focal plane
Each pixel
2. **Faraday rotation modulator (FRM):** BICEP1
 - Modulation using ferrite and coil by Faraday effect
3. **Half-wave plate (HWP):** MAXIPOL, EBEX, SA, SO, ACTPOL, NIKA, LSPE/SWIPE, LiteBIRD...
 - Modulation by rotating HWP ➔ Install at aperture or within optical system
Entire focal plane
4. **Variable-delay polarization modulator:** PIPER, CLASS



QUIET Collaboration et al. (2011)



S. Moyerman et. al. (2013)



A. Kusaka et. al. (2014)

Do we need polarization modulator for LiteBIRD?

Pros	Cons
1/f noise rejection Systematics mitigation	HWP systematics Sensitivity effect System risk

- LiteBIRD $f_{\text{scan}} = 0.05 - 0.1 \text{ rpm}$
- Do we have any guarantee for 1/f noise?
- 1/f is the main driver \rightarrow continuously rotating HWP
- ABS, POLARBEAR successfully demonstrated $f_{\text{knee}} \sim 2 \text{ mHz}$.
- Concerns depend on hardware and calibration.

HWP systematics

Hardware development directly connects to systematics due to HWP imperfection

- HWP non-uniformity → AR and AHWP development
- Multiple reflections → AR development
- HWP phase freq. dependence → AHWP design optimization
- Beam effect through HWP → AR and AHWP development
- HWP temperature stability → rot. mech. thermal characteristics
- HWP wobbling → rot. mech. misalignment
- Angle reconstruction accuracy → encoder
- ...

HWP hardware development is key to achieve LiteBIRD full success

Continuously rotating HWP history

MAXIPOL (balloon)

- First CMB experiment using rotating HWP

EBEX (balloon)

- First experiment using cold rotating HWP with superconducting magnetic bearing

ABS (ground)

- First ground experiment with warm rotating HWP

Simons Array, Simons Observatory SAT (ground)

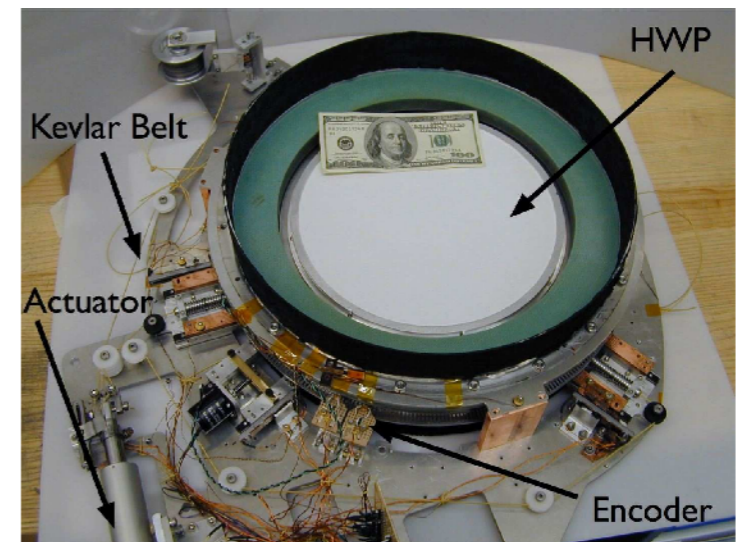
- First ground experiment with cold rotating HWP

LSPE/SWIPE (balloon)

- Balloon experiment with cold rotating HWP

LiteBIRD (satellite)

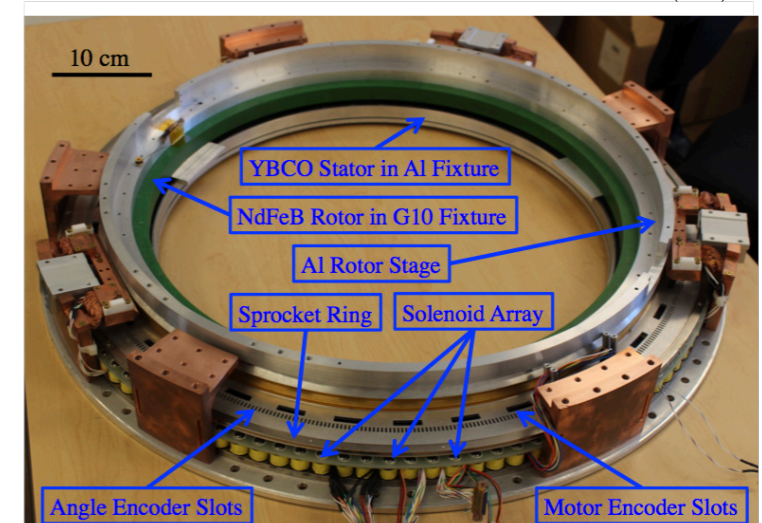
- Satellite mission with cold rotating HWP



J. Klein et. al. Proc. SPIE 8150 (2011)



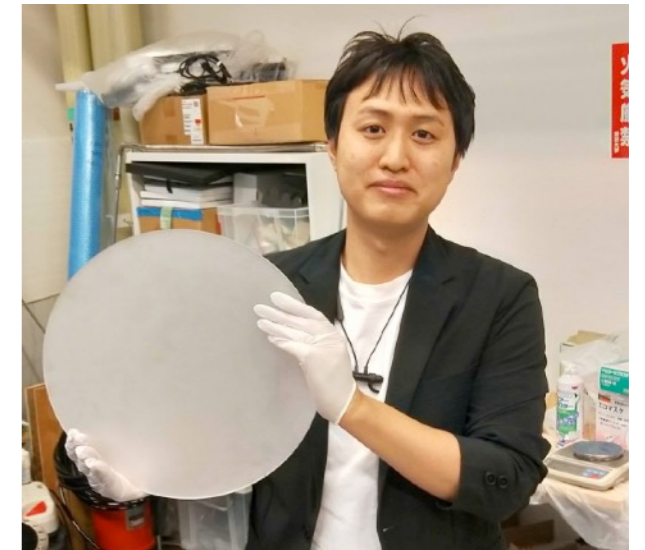
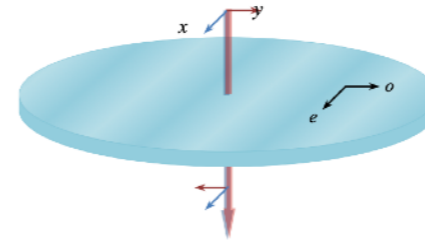
A. Kusaka et. al.(2013)



HWP materials

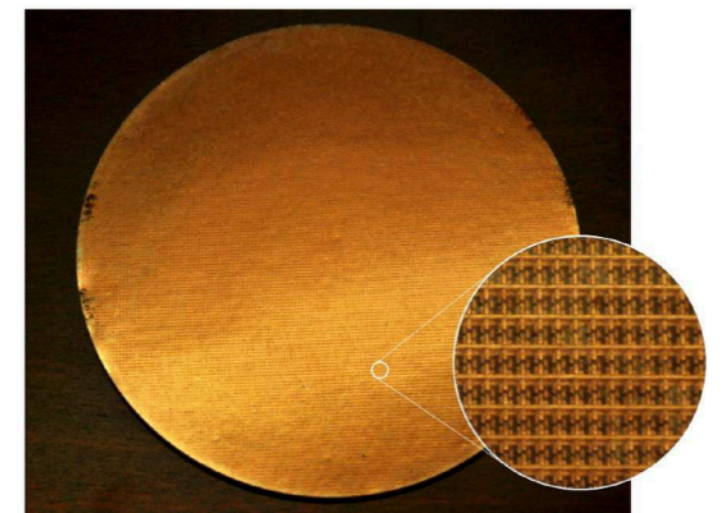
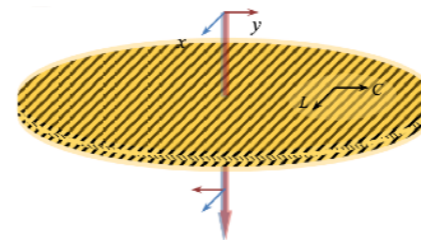
Sapphire

- Birefringence single crystal material
- Maximum diameter $\leq 500\text{mm}$
- Need anti-reflection (AR) due to refractive index ~ 3.3
- Broadband of pol. eff. and phase difference are proportional to number of layer \approx mass
- MAXIPOL, EBEX, SPIDER, ABS, SA, SO, LiteBIRD LFT



Metal-mesh HWP

- Based on metal-mesh filter technology
- Stack capacitive and inductive structure
- Bandwidth 3:1
- NIKA, ASTE, LSPE/SWIPE, LiteBIRD MHFT
- Reflective metal-mesh HWP is considered as backup solution.



G. Pisano et al. in press in PIER M (2012)

Toward satellite application

Higher science goal

- Wider frequency band
- Lower HWP temperature
- Reducing HWP imperfection

Resource limitation

- Cooling power
- Mass
- Volume ...

Space specific environment

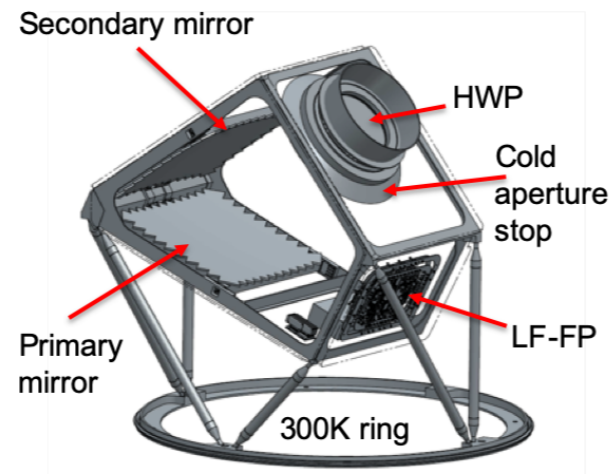
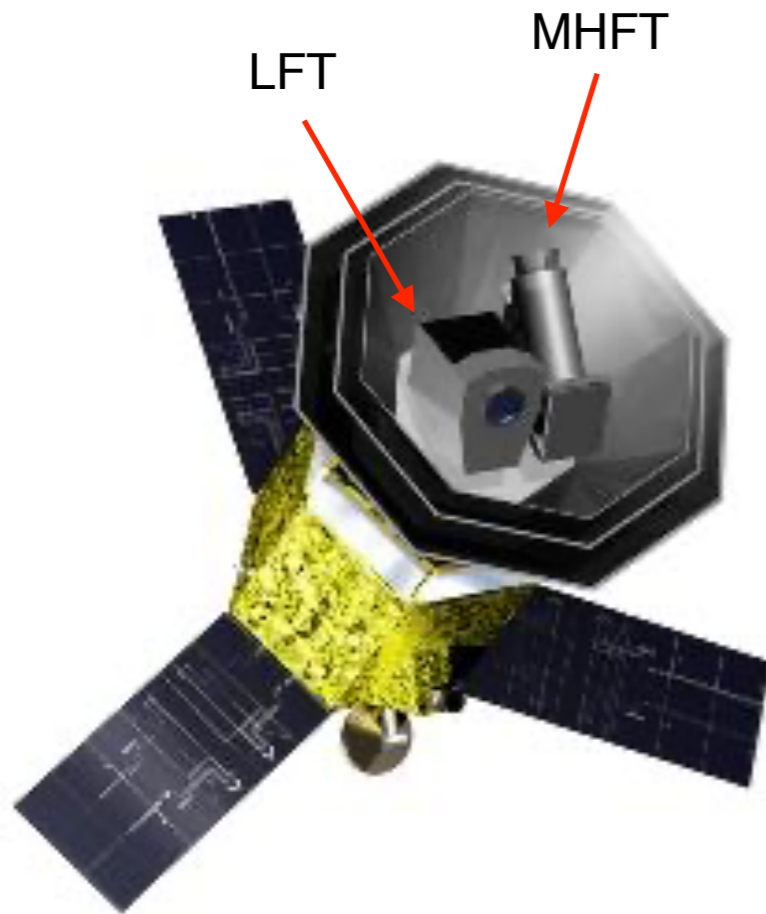
- Launch tolerance
- Cosmic ray
- No gravity

System reliability

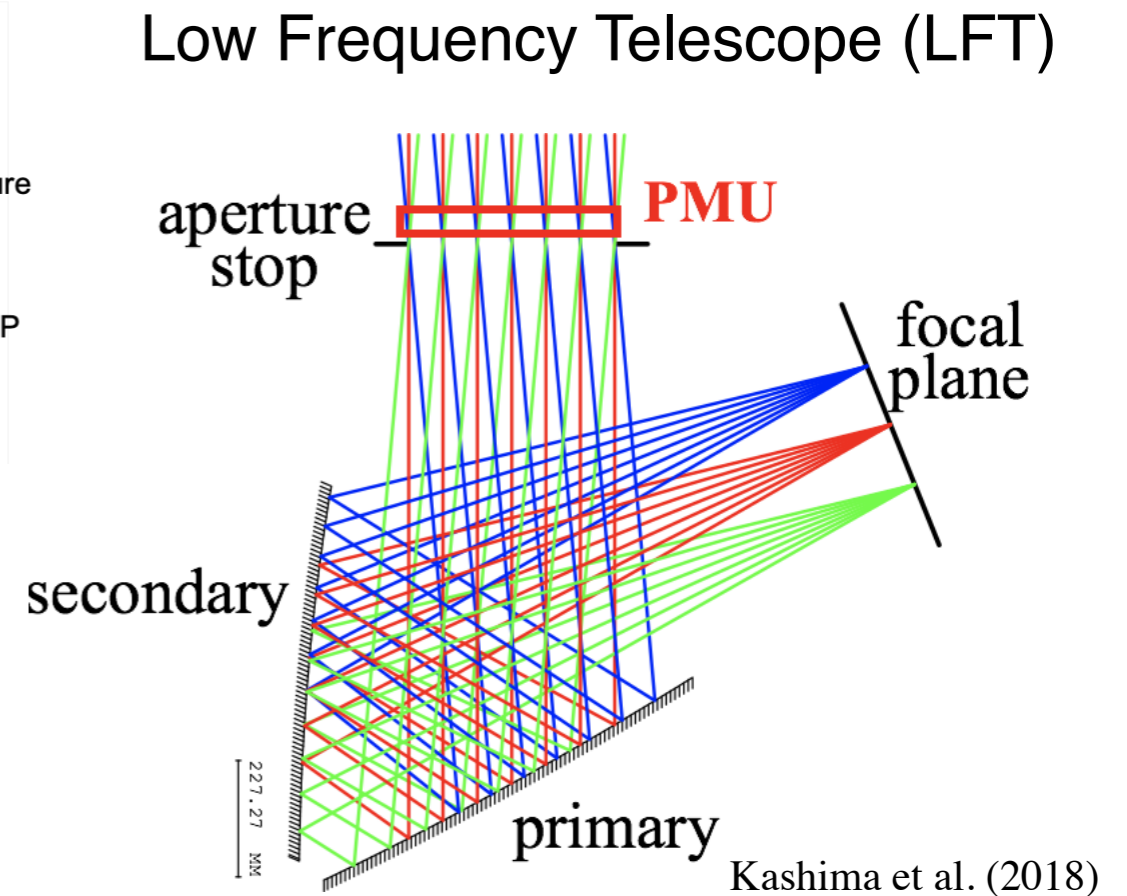
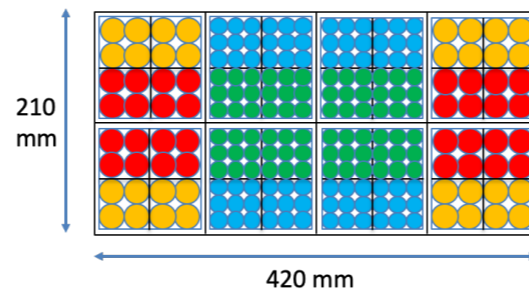
- Risk management
- Redundancy
- Emergency operation

Polarization modulation unit (PMU) for LiteBIRD low frequency telescope (LFT)

LiteBIRD overview



Sugai et al. (2019)



Two telescopes : LFT (34 - 161GHz), MHFT (89 - 448GHz)

Focal plane unit : >4000 superconducting detector (TES) array

Scan strategy : L2 precession 45 deg. (10^{-2} - 10^{-3} rpm), spin 50 deg. (0.05-0.1 rpm)

Cooling chain : V-groove → 20K-2ST → 4.8K-JT → 1.75K ADR → 300/100mK ADR

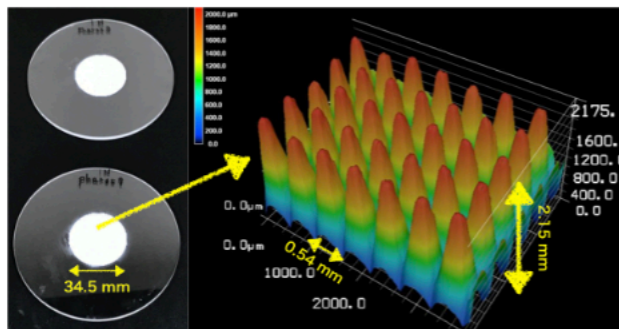
Continuous rotating half-wave plate at the aperture of LFT and MHFT

Representative requirements

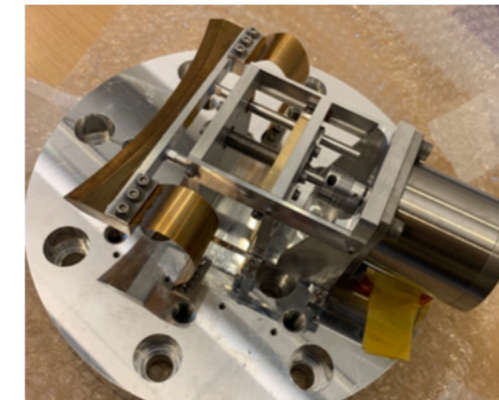
Items	Requirement (LFT)
Frequency band	34 GHz - 161 GHz
Transmittance	> 98% (depend on freq.)
Polarization efficiency	> 98% (depend on freq.)
Rotation frequency	0.8 Hz (48 RPM)
HWP diameter	> ~ 480 mm
HWP temperature	< 20 K
Total heat dissipation	< 4 mW
Mass	< 30 kg
Encoder specification	< 0.2 arcmin

- ✓ The requirement values are not yet fixed because the detail system design and the trade-off study are in progress.
- ✓ Main development items are **broadband achromatic HWP** and a **cryogenic rotation mechanism**.

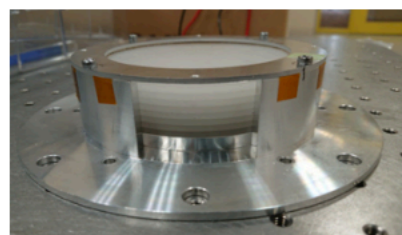
Current design of LiteBIRD LFT PMU



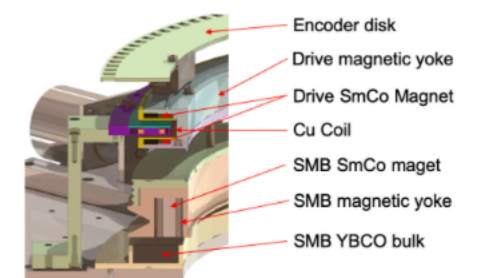
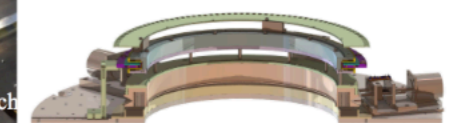
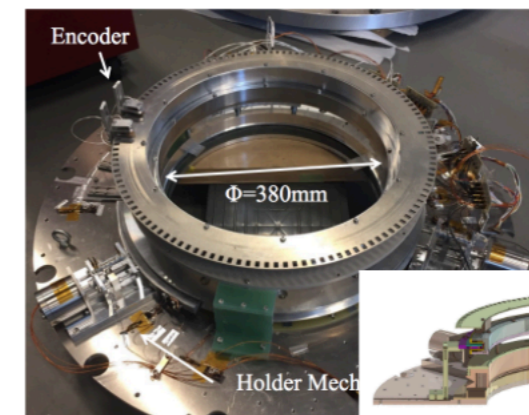
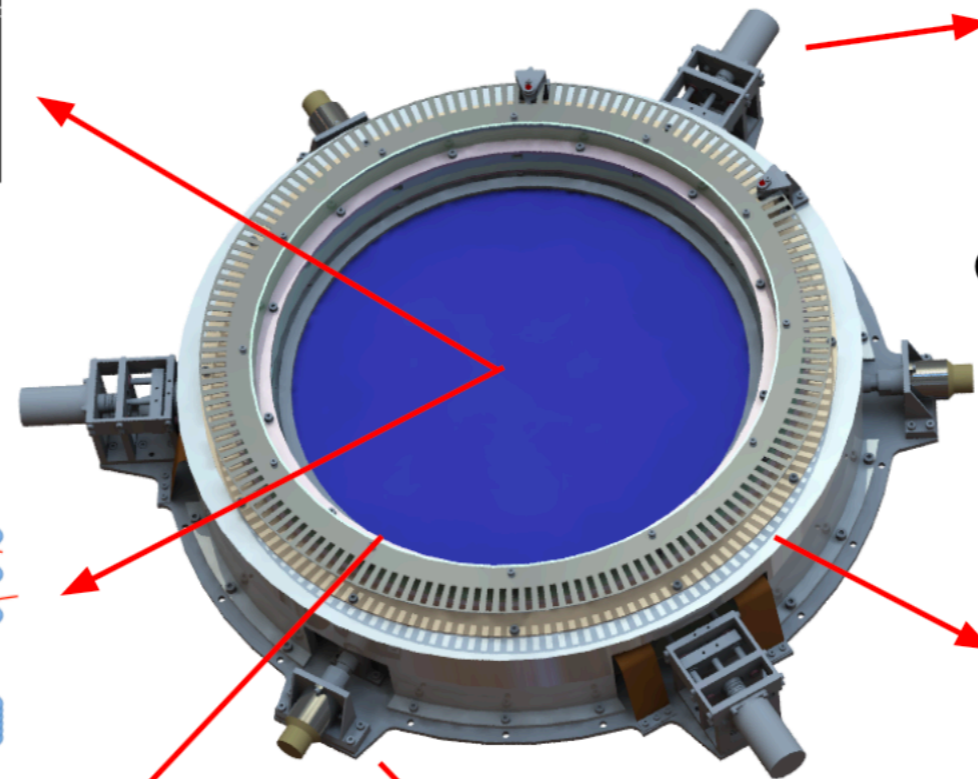
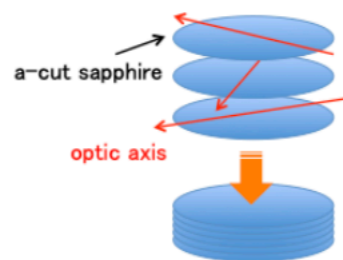
Anti-reflection structure



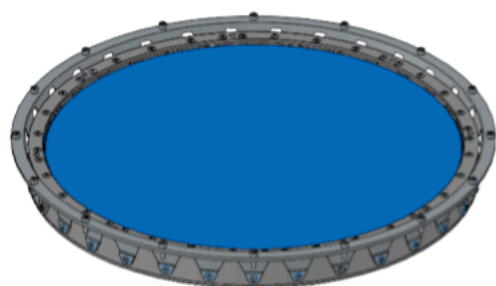
Cryogenic holder mechanism



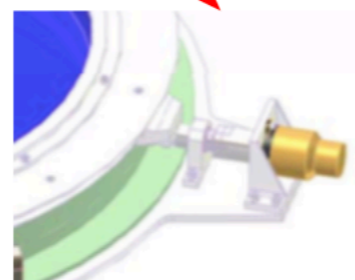
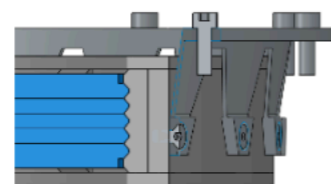
Sapphire stacked Achromatic HWP



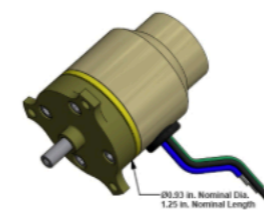
Rotation mechanism



HWP holder



Launch lock mechanism



Development roadmap

~2020

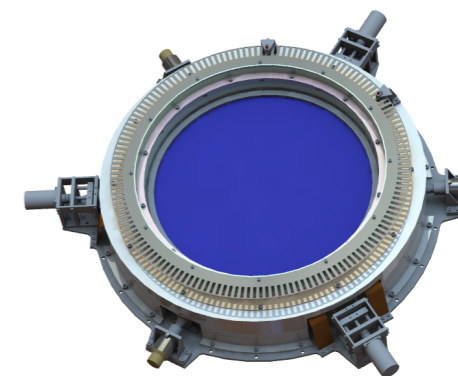
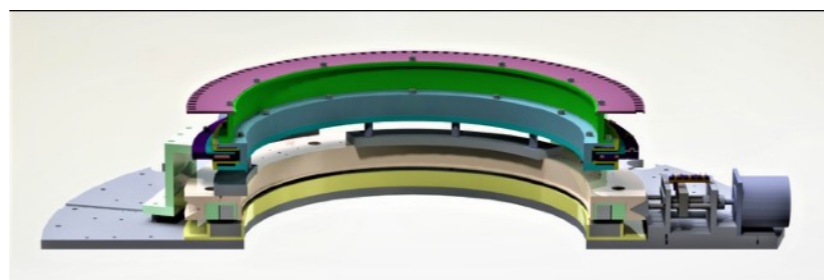
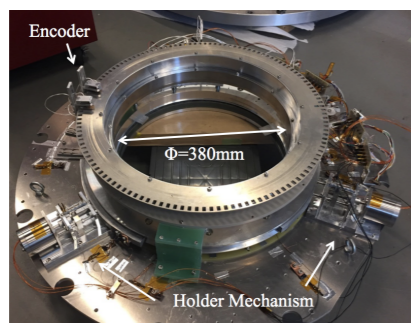
2020~2024

2024~launch!

BBM
 $\Phi=380\text{mm}$

DM/EM
 $\Phi=500\text{mm}$

FM
 $\Phi=500\text{mm}$

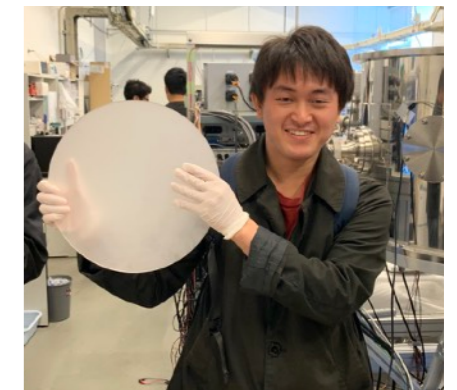
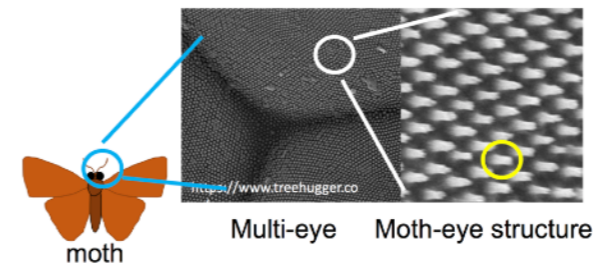


	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027
Project phase		Phase A			Phase B	Phase C		Phase D		
BBM performance test	█	█								
DM procurement		█	█	█						
DM performance test			█	█						
DM integration test			█	█	█					
DM to EM						█	█	█		
FM procurement							█	█		
FM performance test								█	█	
FM integration test									█	█

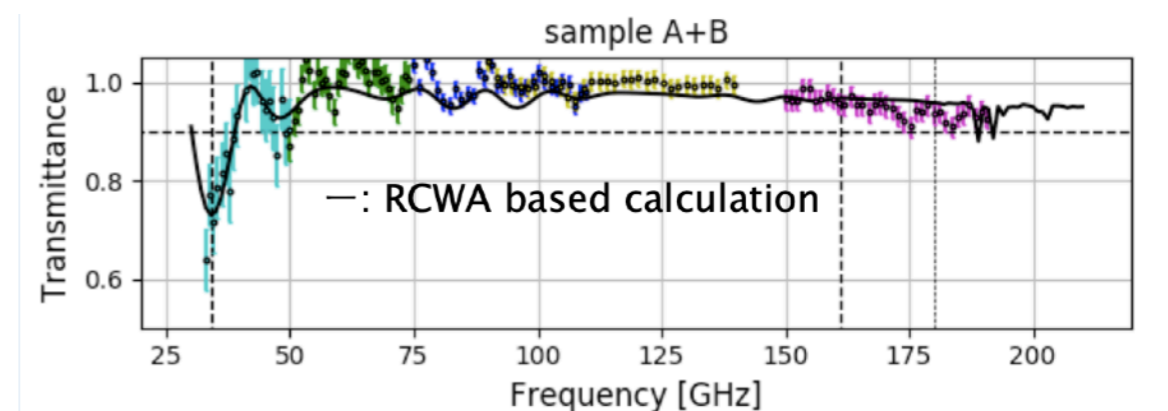
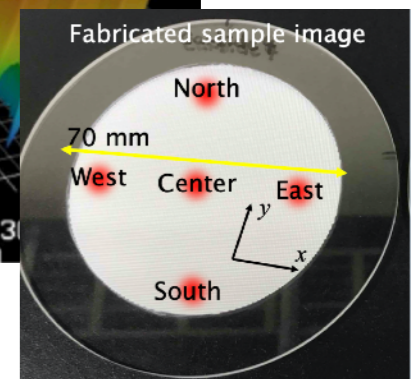
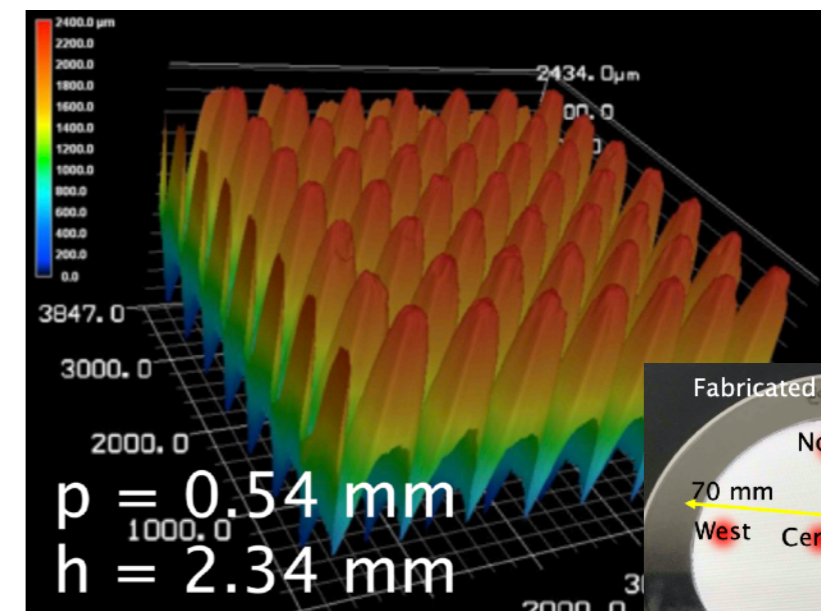
Preliminary

Broadband anti-reflection structure

- Broadband antireflection (34-161GHz): moth-eye based sub-wavelength structure by laser machining
- Fabricated $\Phi 70\text{mm}$ small sample with height 2.34mm, pitch 0.54mm ($\sim 4:1$)
- $> 90\%$ transmittance with good agreement between data and simulation
- The expected processing time for $\Phi=450\text{mm}$ is < 1 month using 40W femto-second pulsed laser

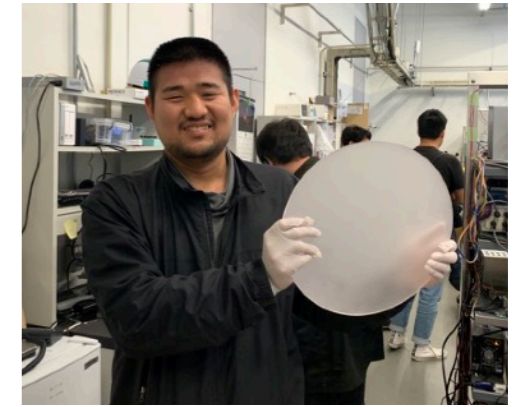


Ryota Takaku (U. Tokyo)

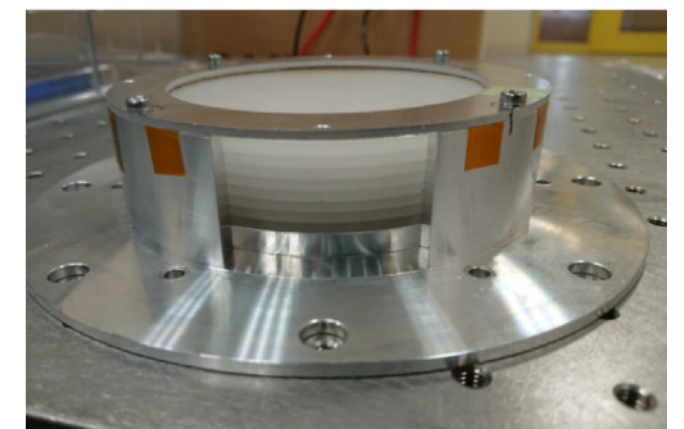
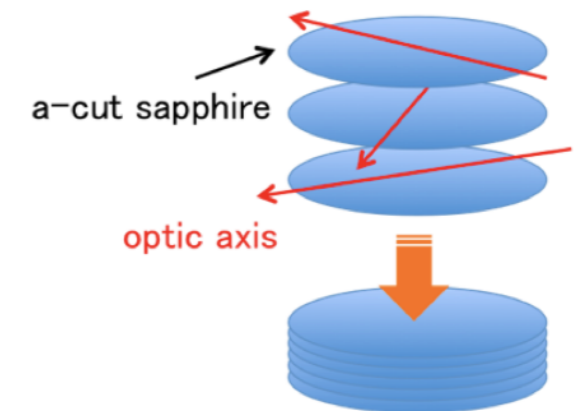


Sapphire AHWP development

- ✓ Single sapphire plate has pol. eff. $\varepsilon = 1$ for the only single frequency.
- ✓ We adopt Achromatic HWP (AHWP) consists of multi-stacked sapphire with the different optic axis for each HWP.
- ✓ We optimize the AHWP design with 5 layer to cover 34-161GHz.

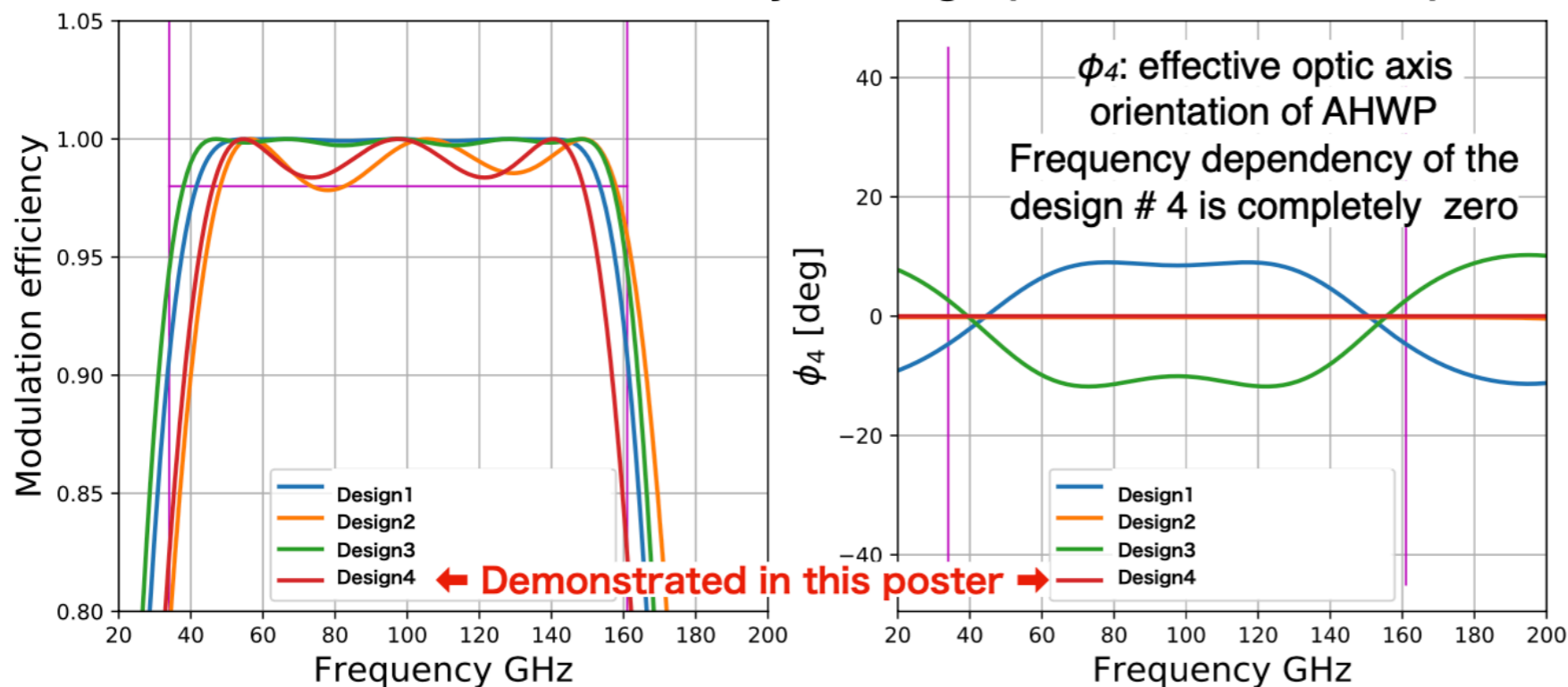


Kunimoto Komatsu (Okayama U.)



K. Komatsu et al. (2019)

Prediction of each five-layer design (w/o reflection effect)



Rotation mechanism

- All components at 5 K stage
- Heat dissipation < 4 mW due to cooling power
- Rotor (HWP) must be operated < 20 K to reduce thermal emission

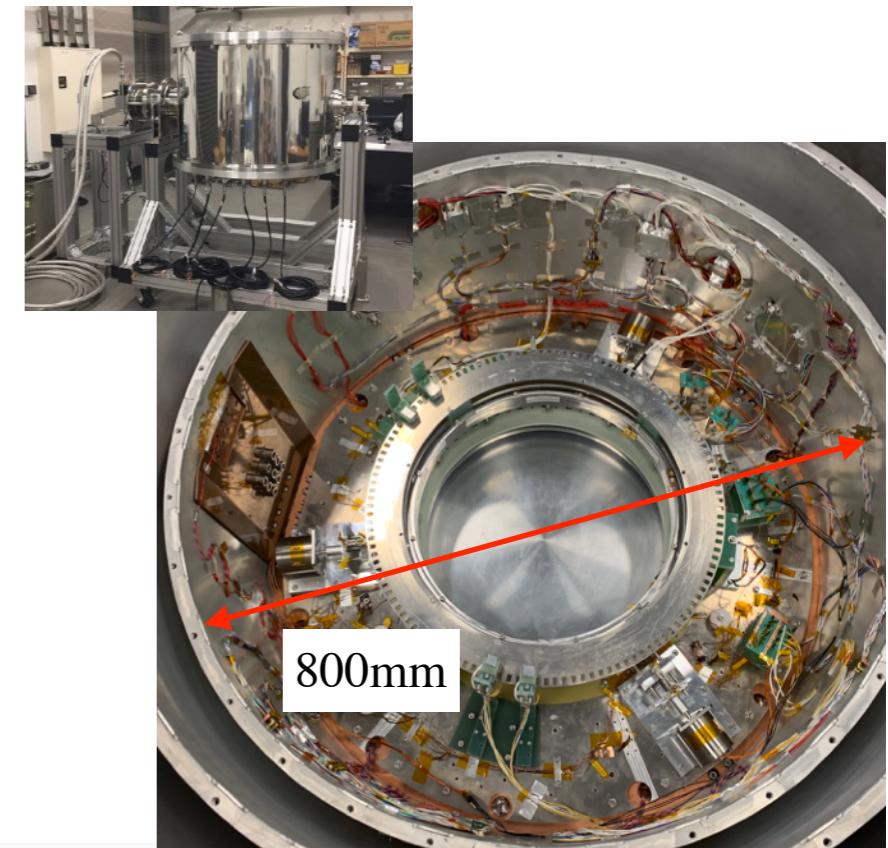


Stable continuous rotation at cryogenic temperature with small heat dissipation

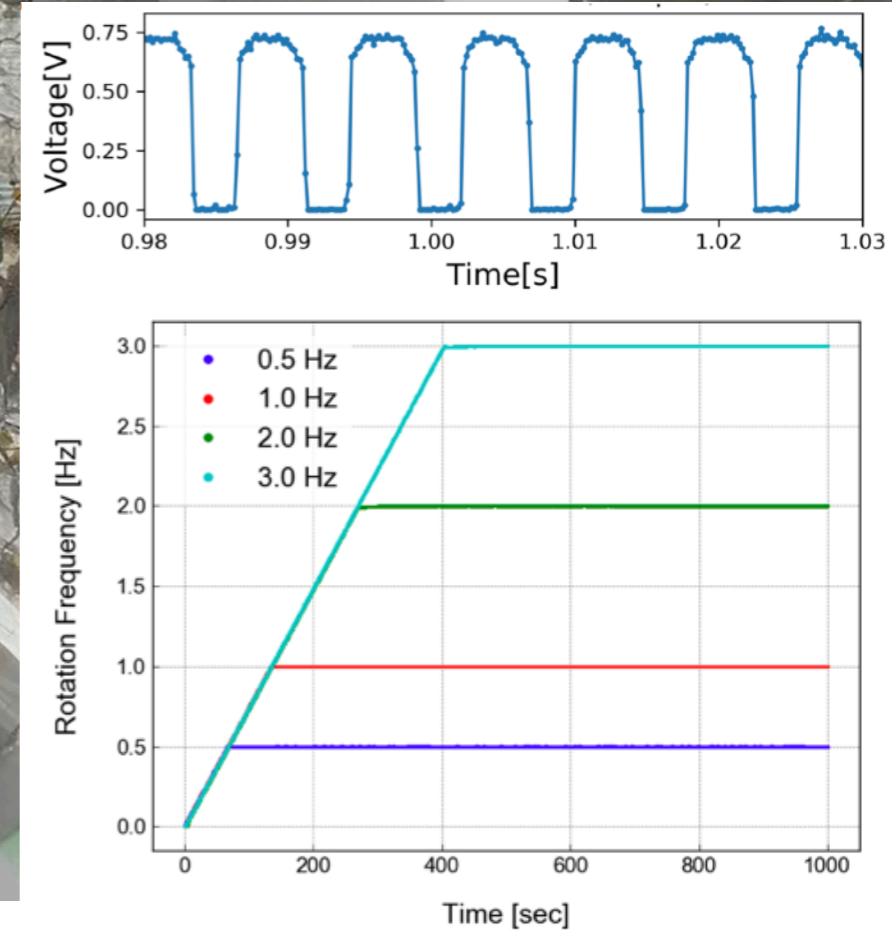
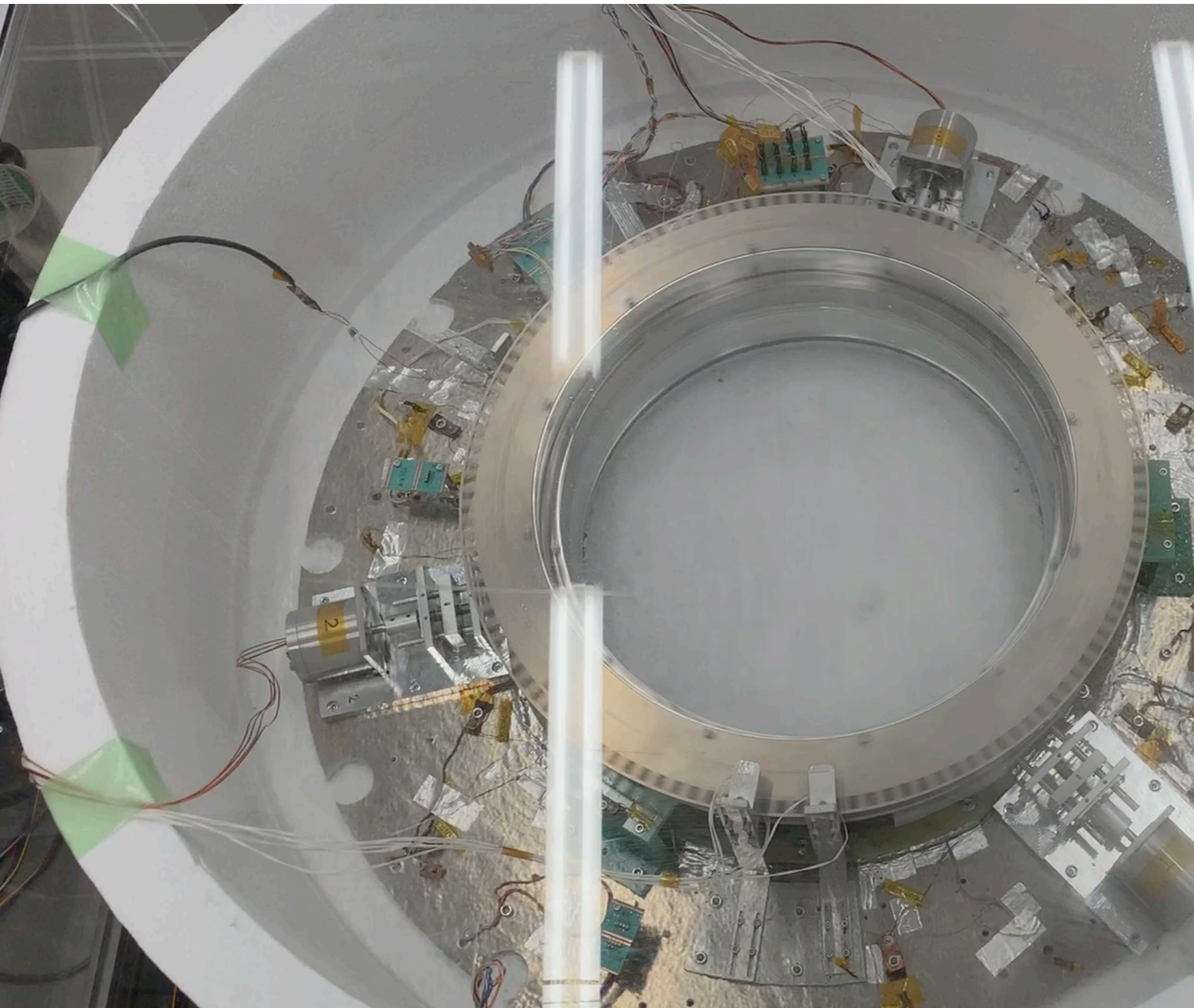


Breadboard model ($\Phi=380$ mm)

- Superconducting magnetic bearing
Rotor: SmCo magnets + yoke for uniformity
Stator: YBCO ($T_c < 95$ K)
- DC brushless motor with speed feedback control measured by optical encoder
- 3 grippers actuated by linear actuators (stepping motors)



Rotation mechanism



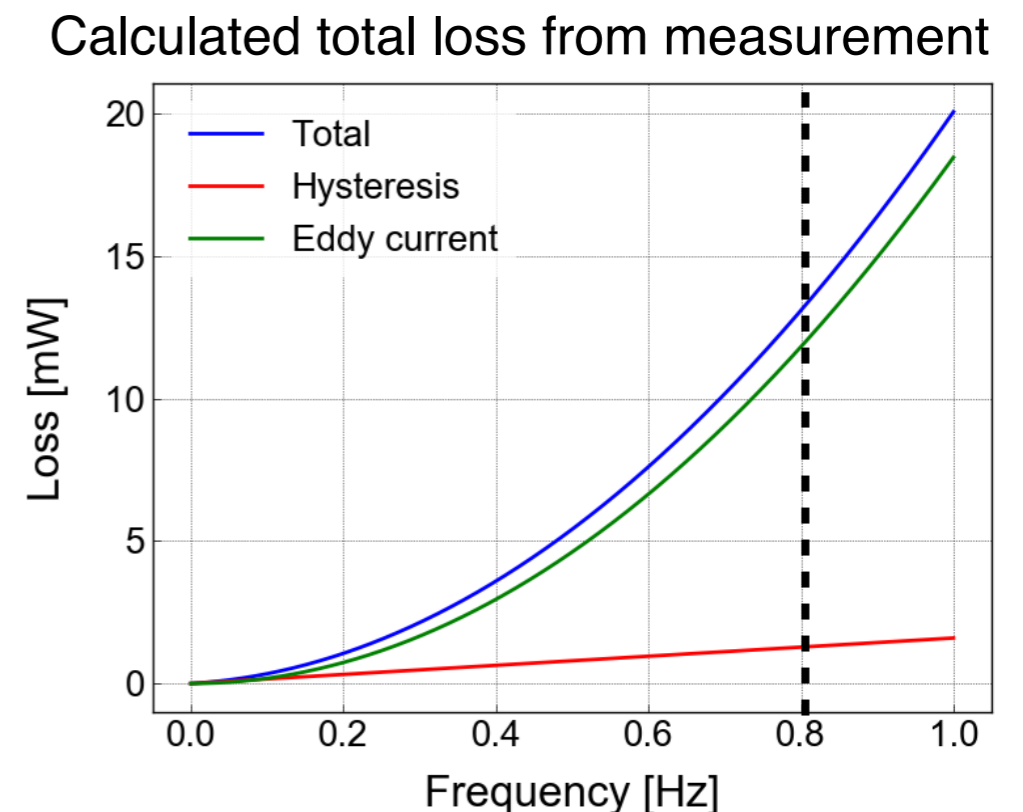
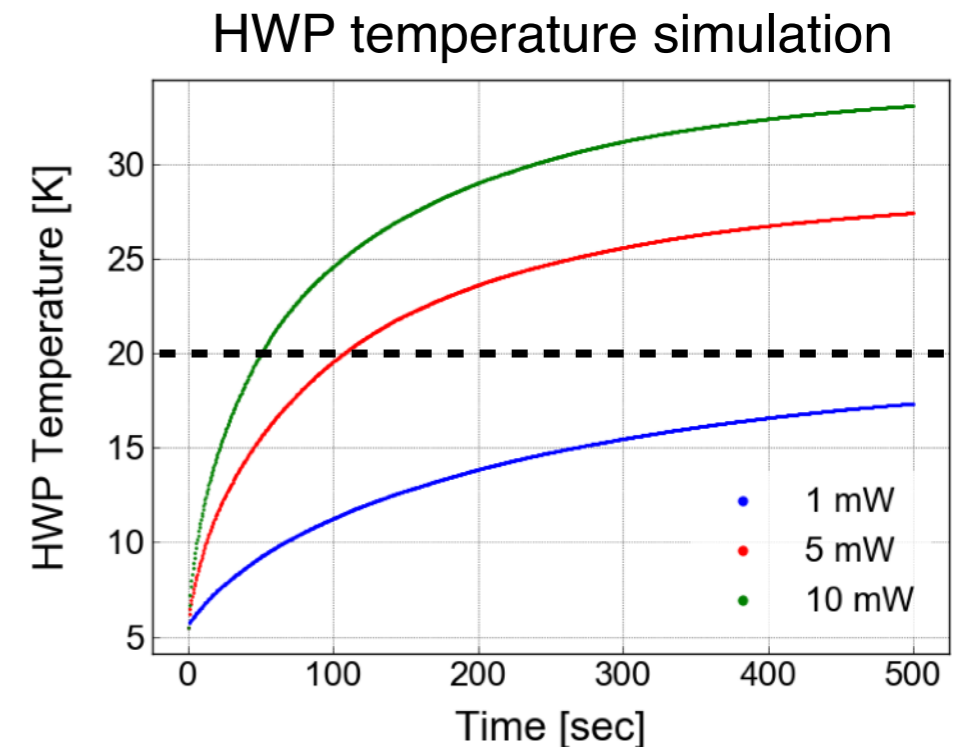
Thermal characteristics

- Total heat dissipation ≤ 4.0 mW
- Rotor heat dissipation ≤ 1.0 mW from thermal simulation
- Heat sources are hysteresis loss, eddy current due to magnet inhomogeneity ΔB

$$P_h \propto k_h f \frac{\Delta B^3}{J_c}, P_e \propto k_e f^2 \Delta B^2$$

- Total loss at nominal rotation speed (46 rpm) is ~ 10 mW, dominated by eddy current loss
- There is much room for improvement.
 - de-metallization, reduce weight ...
 - Uniform magnet with yoke

Yoshiki Nomura (Saitama U.)

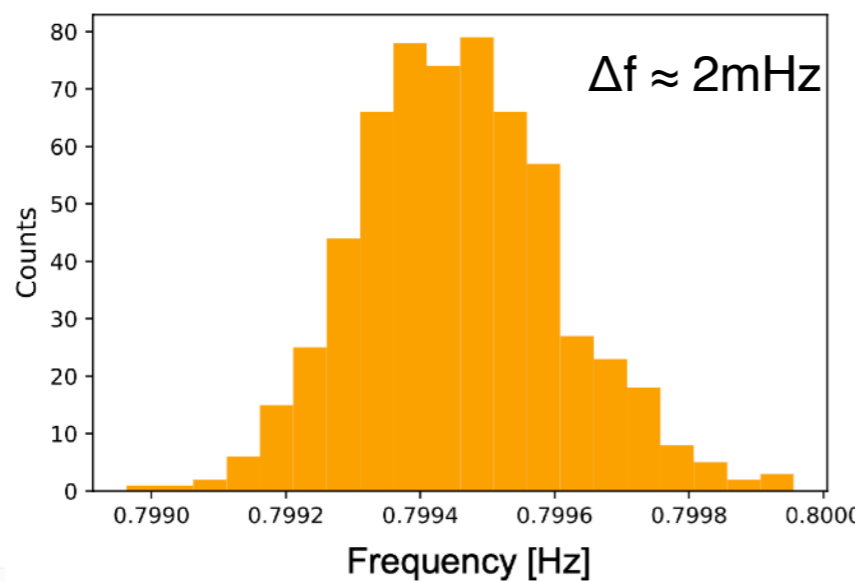
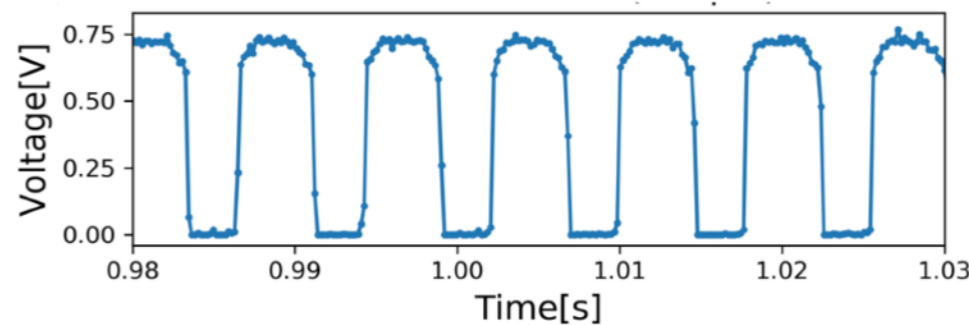
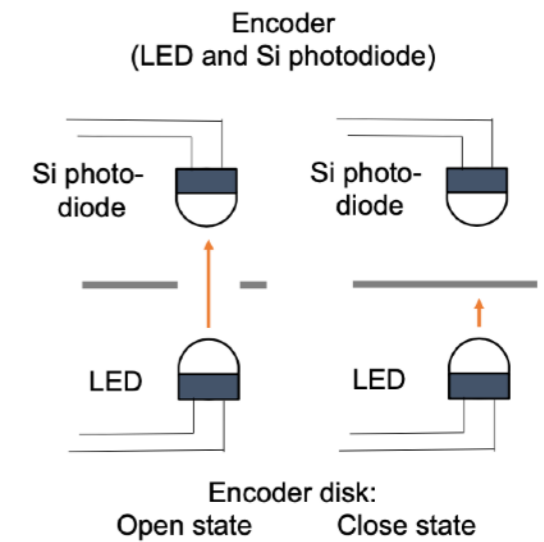


Angular encoding

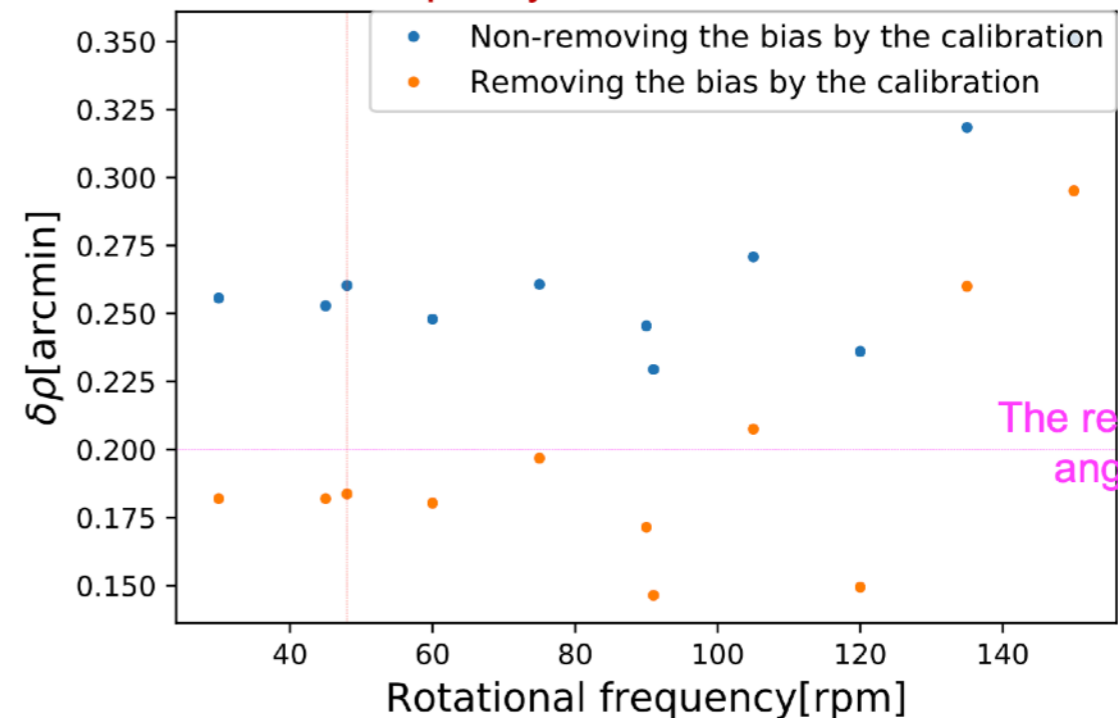


Shinya Sugiyama (Saitama U.)

- HWP angle reconstructed by incremental encoder consists of LED and Si photodiode
- Calibrate bias component (not change with each rotation).
- The angular error (random component changed per rotation) is calculated as < 0.2 arcmin.

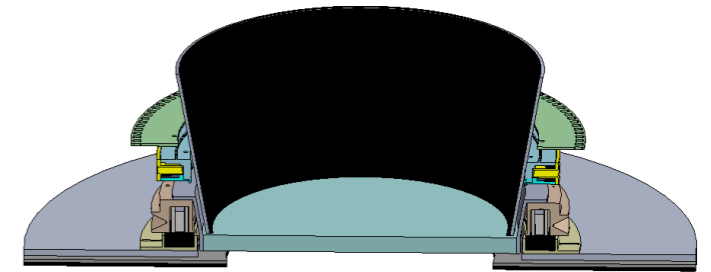


The target of a rotational frequency



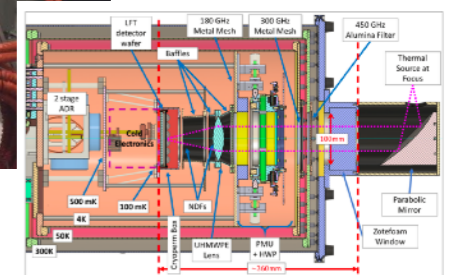
Other activities toward flight model

- Cosmic ray effect: radiation damage, heat input, charging
- AHWP gluing and holder design for launch tolerance.
- System optimization including baffle and stop
- Fault tree analysis (FTA) to identify critical risks and components required redundancy.
- Development of low loss cryogenic motor
- Cryogenic optical measurement system
- Small integrated test system of TES and HWP



ADR testbed

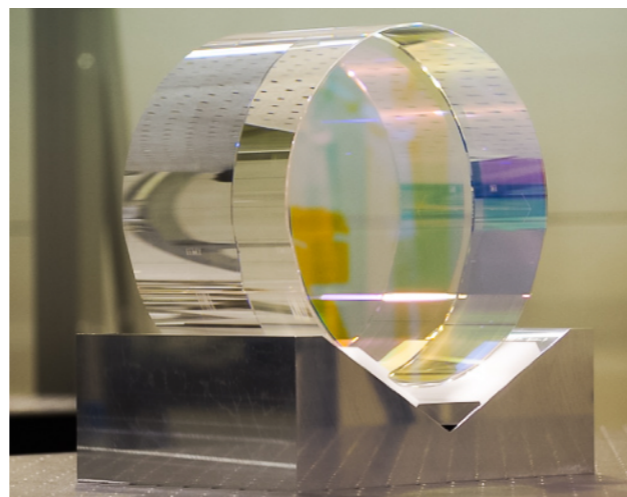
T. Ghigna et al (2019)



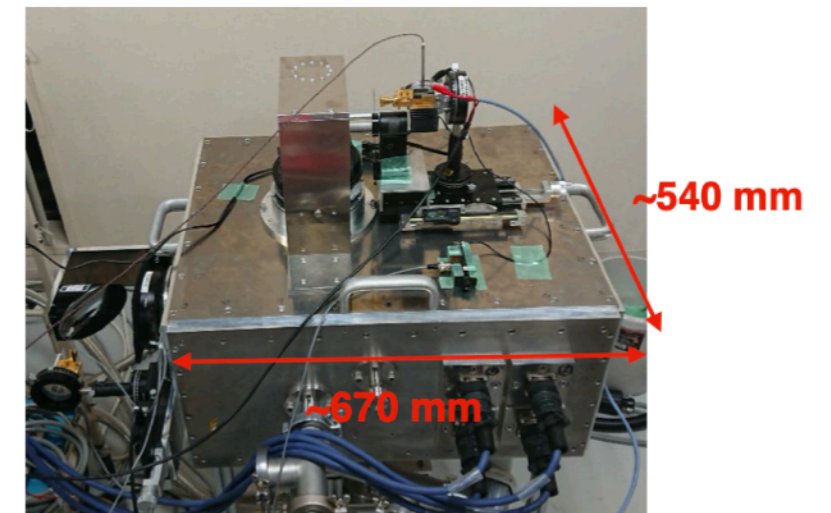
Cosmic ray test @ HIMAC



Sapphire Gluing (KAGURA)



4K CM cryostat @ Kavli IPMU



Summary

- ✓ Polarization modulator helps to reject $1/f$ noise and systematics.
- ✓ Continuously rotating HWP is employed to LiteBIRD with the main driver as $1/f$ noise.
- ✓ We presented the development status of LiteBIRD LFT PMU.
- ✓ Optical performance of AR and AHWP is successfully demonstrated by small samples.
- ✓ Cryogenic performance test of BBM rotation mechanism is in progress toward flight model.

Otsukare!

