Table 1: Summary of important quantities for all models in relativistic (R) and Newtonian (N) gravity. t_b is the time of bounce, $\rho_{\mathrm{max\,b}}$ is the maximum density at bounce, $|A_{20}^{\mathrm{E2}}|_{\mathrm{max}}$ is the maximum gravitational wave amplitude, ν_{max} is the frequency of maximum spectral energy density, $\beta_{\mathrm{rot\,max}}$ is the maximum rotation rate, $\rho_{\mathrm{max\,f}}$ is the maximum density after ring-down, and Type specifies the collapse type. If the maximum density is located off-center, the respective density value is marked with an asterisk. For models of type II or I/II, $\rho_{\mathrm{max\,f}}$ cannot be determined.

Model	t_b	$\rho_{\mathrm{max\,b}}$	$\frac{\rho^{\mathrm{R}}_{\mathrm{max\,b}}}{\rho^{\mathrm{N}}_{\mathrm{max\,b}}}-1$	$\lvert A_{20}^{\mathrm{E2}}\rvert_{\mathrm{max}}$	$\frac{\lvert A_{20}^{\mathrm{E2}}\rvert^{\mathrm{R}}_{\mathrm{max}}}{\lvert A_{20}^{\mathrm{E2}}\rvert^{\mathrm{N}}_{\mathrm{max}}}-1$	ν_{max}	$\frac{\nu^{\mathrm{R}}_{\mathrm{max}}}{\mu^{\mathrm{N}}_{\mathrm{max}}}-1$	$\beta_{\mathrm{rot\,max}}$	$\frac{\beta^{\mathrm{R}}_{\mathrm{rot\,max}}}{\beta^{\mathrm{N}}_{\mathrm{rot\,max}}}-1$	$\rho_{\mathrm{max\,f}}$	Type
	[ms]	$\left[10^{14}\,\frac{\mathrm{g}}{\mathrm{cm}^3}\right]$	[%]	[cm]	[%]	[Hz]	[%]	[%]	[%]	$\left[10^{14}\,\frac{\mathrm{g}}{\mathrm{cm}^3}\right]$	
A1B1G1$^\mathrm{R}$	91.22	4.65	+44	950	−44	602	+17	4.0	−23	3.3	I
A1B1G1$^\mathrm{N}$	92.23	3.22		1698		515		5.2		—	I/II
A1B2G1$^\mathrm{R}$	91.91	4.32	+49	1795	−24	618	+39	6.9	−16	3.1	I
A1B2G1$^\mathrm{N}$	93.10	2.89		2355		446		8.2		—	II
A1B3G1$^\mathrm{R}$	93.20	3.85	+77	2694	+84	1262	+554	11.5	+7	2.7	I
A1B3G1$^\mathrm{N}$	94.70	2.17		1463		193		10.7		—	II
A1B3G2$^\mathrm{R}$	69.42	3.99	+41	1723	−17	654	+46	9.7	−8	2.8	I
A1B3G2$^\mathrm{N}$	69.87	2.83		2084		448		10.6		—	II
A1B3G3$^\mathrm{R}$	48.64	4.16	+23	663	−32	675	+17	7.7	−4	3.0	I
A1B3G3$^\mathrm{N}$	48.57	3.38		976		576		8.0		2.5	I
A1B3G5$^\mathrm{R}$	30.21	4.49	+5	124	−5	876	+3	4.2	+24	3.2	III
A1B3G5$^\mathrm{N}$	29.98	4.26		131		852		3.4		3.0	III
A2B4G1$^\mathrm{R}$	99.69	0.64	+482	522	−20	80	+31	15.6	+32	—	II
A2B4G1$^\mathrm{N}$	99.71	0.11		652		61		11.8		—	II
A3B1G1$^\mathrm{R}$	91.68	4.44	+48	1954	−22	977	+103	6.8	−9	3.1	I
A3B1G1$^\mathrm{N}$	92.72	3.00		2510		482		7.5		—	II
A3B2G1$^\mathrm{R}$	92.85	3.90	+71	2845	+66	734	+61	12.2	+11	2.7	I
A3B2G1$^\mathrm{N}$	94.32	2.28		1711		456		11.0		—	II
A3B2G2$^\mathrm{R}$	69.50	3.88	+45	2141	−11	750	+52	11.6	−1	2.8	I
A3B2G2$^\mathrm{N}$	69.98	2.68		2407		494		11.7		—	II
A3B2G4$^\mathrm{R}_\mathrm{soft}$	39.33	5.81	+31	597	−24	870	+15	10.3	+8	3.3	I
A3B2G4$^\mathrm{N}_\mathrm{soft}$	39.14	4.45		781		755		9.5		2.7	I
A3B2G4$^\mathrm{R}$	39.35	3.97	+16	506	−28	806	+9	9.6	+7	2.8	I
A3B2G4$^\mathrm{N}$	39.07	3.41		703		737		9.0		2.5	I
A3B3G1$^\mathrm{R}$	95.44	3.03	+545	1035	−5	482	+161	19.0	+65	—	II
A3B3G1$^\mathrm{N}$	96.57	0.47		1087		185		11.5		—	II
A3B3G2$^\mathrm{R}$	71.15	3.10	+182	1305	−8	501	+83	18.7	+36	—	I/II
A3B3G2$^\mathrm{N}$	71.77	1.10		1420		274		13.7		—	II
A3B3G3$^\mathrm{R}$	49.66	3.14	+32	1255	−15	764	+110	17.7	+13	—	I/II
A3B3G3$^\mathrm{N}$	49.64	2.38*		1480		363		15.7		—	I/II
A3B3G5$^\mathrm{R}$	30.66	3.67	+6	256	−3	986	+2	11.8	+27	2.5	III
A3B3G5$^\mathrm{N}$	30.36	3.45*		263		964		9.3		2.3*	III
A3B4G2$^\mathrm{R}$	74.73	0.57	+256	624	−30	92	−8	18.3	+24	—	II
A3B4G2$^\mathrm{N}$	73.99	0.16*		894		85		14.7		—	II
A3B5G4$^\mathrm{R}$	44.42	0.22*	+47	491	−7	89	−21	24.1	+16	—	III
A3B5G4$^\mathrm{N}$	44.31	0.15*		528		113		20.7		—	III
A4B1G1$^\mathrm{R}$	90.82	4.63*	+59	2325	+17	1101	+90	7.4	+0	3.0*	I
A4B1G1$^\mathrm{N}$	91.77	2.92*		1992		580		7.4		—	II
A4B1G2$^\mathrm{R}$	68.38	4.47*	+45	2003	−2	1124	+19	8.7	+2	2.8*	I
A4B1G2$^\mathrm{N}$	68.69	3.09*		2034		946		8.5		—	II
A4B2G2$^\mathrm{R}$	68.63	4.30*	+66	3026	+42	1014	+118	14.4	+14	—	I/II
A4B2G2$^\mathrm{N}$	69.02	2.59*		2132		466		12.6		—	II
A4B2G3$^\mathrm{R}$	48.88	4.01*	+41	2209	−4	890	+141	18.0	+16	—	I/II
A4B2G3$^\mathrm{N}$	48.74	2.85*		2217		370		15.5		—	I/II
A4B4G4$^\mathrm{R}$	40.19	1.23*	+68	925	−47	151	−33	27.1	+20	—	I/II
A4B4G4$^\mathrm{N}$	39.66	0.73*		1748		226		22.6		—	I/II
A4B4G5$^\mathrm{R}$	32.34	2.23*	−1	1212	−44	187	−14	33.9	+21	—	I/II
A4B4G5$^\mathrm{N}$	31.91	2.25*		2149		217		28.0		—	I/II
A4B5G4$^\mathrm{R}$	38.07	0.47*	+24	1828	−38	76	+0	32.0	+15	—	I/II
A4B5G4$^\mathrm{N}$	37.29	0.38*		2965		76		27.9		—	I/II
A4B5G5$^\mathrm{R}$	31.21	1.72*	+42	2629	−31	130	−2	41.1	+22	—	I/II
A4B5G5$^\mathrm{N}$	30.94	1.22*		3818		133		33.7		—	I/II